least 70 N/mm².--

— 5. (New) The process according to claim 3 wherein said bake hardening potential is at least 70 N/mm².--

REMARKS

Favorable reconsideration of the above-identified patent application, as amended herein, is respectfully requested. Claims 1-3 are presently pending. Claims 1-3 were rejected. Of the claims, Claims 1 and 3 are independent. Claims 1 and 3 have been amended to more clearly recite the claimed invention. Specifically, Claims 1 and 3 have been amended to replace the phrases "dressed" with "temper rolled" and "dressing" with "temper rolling." The Iron and Steel Dictionary and Metals Handbook entries attached hereto as Exhibit A demonstrate that it is known in the art that "dressing" means "temper rolling", and that temper rolling is a process known in the art for suppressing and/or removing yield point elongation. Specifically, the Iron and Steel Dictionary illustrates that "to dress" means "temper rolling". The Metals Handbook at pp. 205-206 and 693 demonstrates that temper rolling is a process known in the art to be effective for suppressing and/or removing yield point elongation.

The §112, Second Paragraph Rejection

Claims 1-3 were rejected under 35 U.S.C. § 112, second paragraph, as being indefinite for failing to particularly point out and distinctly claim the subject matter of the invention. It is respectfully submitted that the rejection of Claims 1 and 3 for reciting the phrase "non-ageing steel" is improperly based on the claims as originally filed, and not on the claims as amended on September 29, 1999. This amendment resulted in, *inter alia*, removing the phrase "non-

ageing steel." In view of this amendment, Applicants deem this rejection to be moot.

Applicants respectfully submit that the Examiner's rejection of Claim 1 for reciting the phrase "dressed strip" and of Claim 3 for reciting the phrase "cold rolled and dressed" is also improperly based on the claims as originally filed, and not on the claims as amended on September 29, 1999. This amendment removed both the phrases "dressed strip" and "cold rolled and dressed." In view of this amendment, Applicants deem this rejection to be moot.

The Examiner rejected Claims 1 and 3 under 35 U.S.C. § 112, second paragraph, as being indefinite for reciting the phrase "stove finished." The Examiner asserts that this term is not known to one of ordinary skill in the art, nor distinctly defined in the instant specification. Applicants respectfully submit that such phrase is known to the ordinary artisan. As defined in an English-German Dictionary of Engineering and Technology (attached hereto as Exhibit B), "stove finish" is synonymous with "stove enamel" and "stove drying." One of ordinary skill in the art would thus understand that "stove finished" means "stove enamelling" or "stove drying" of the strip to utilize the bake-hardening potential.

The Examiner further rejected Claims 1 and 3 under 35 U.S.C. § 112, second paragraph, as being indefinite for reciting the broad recitation "high bake-hardening potential" along with "more particularly of more than 70 N/mm²." The phrase "more particularly of more than 70 N/mm²" has been removed from Claims 1 and 3 and incorporated into new Claims 4 and 5. In view of such amendments, Applicants deem the rejection under 35 U.S.C. § 112, second paragraph, to be obviated and respectfully request withdrawal thereof.

The §103 Rejection

Claims 1 - 3 were rejected under 35 U.S.C. §103(a) as being unpatentable over

Stevenson (U.S. Patent No. 4,358,325, hereafter "Stevenson"). For a rejection to be sustained under 35 U.S.C. §103(a), the differences between the features of the reference and the claimed invention must have been obvious to one skilled in the art at the time of the invention.

The Examiner asserts that Stevenson teaches a process for making a steel strip with improved formability comprising hot or cold rolling, cooling to a temperature below room temperature and forming as presently claimed in Claim 1. The Examiner further asserts that Stevenson teaches that a steel strip can be retained at room temperature for approximately a week prior to forming as presently claimed in Claim 3. The Examiner acknowledges that Stevenson does not teach bake hardenability of a strip that has been processed according to the instant invention, but asserts that because Stevenson teaches substantially the same method as presently claimed, substantially the same results, i.e., bake hardening, would occur.

It is respectfully submitted that one of ordinary skill in the art would not have been motivated by the teachings of Stevenson to arrive at the instant invention. Firstly, unlike the presently claimed invention, Stevenson does not disclose a maximum value for the condition $R_{ch}-R_{cl}$. Additionally, Stevenson does not disclose or suggest storing of a cold strip, which is cold rolled under usual conditions, at temperatures below room temperature. This is in direct contrast with the instant invention which discloses a method of cold rolling an ageing-sensitive steel strip under normal conditions, followed by storage at temperatures below room temperature.

Furthermore, unlike the instant invention, Stevenson does not disclose or suggest the dependency between the temperature and time of storage and the effect of these two parameters on ageing. In light of these substantial differences, Applicants respectfully submit that Stevenson does not teach substantially the same method as presently claimed and that one of

ordinary skill in the art would not have been motivated to modify the teachings of Stevenson to arrive at the instantly claimed invention.

Claim 3 was rejected under 35 U.S.C. §103(a) as being unpatentable over Nakaoka (U.S. Patent No. 4,050,959, hereafter "Nakaoka"). The Examiner states that Nakaoka teaches a method for producing a non-ageing steel sheet with high formability at the forming stage, and high hardness at the coat-baking stage. The Examiner asserts that because Nakaoka teaches substantially the same method as instantly claimed, as well as a bake hardenability within the presently claimed range, Nakoaka renders the instant invention obvious.

Applicants respectfully submit that the ordinary artisan would not have been motivated to modify the teachings of Nakoaka to arrive at the instant invention. Claim 3 is directed to a process for the production of a buckling-resistant stove-finished structural component from ageing-sensitive steel while preventing ageing of the steel. Nakaoka, on the other hand, teaches production of a non-ageing steel, and not the prevention of ageing of an ageing-sensitive steel.

Additionally, unlike the presently claimed invention, Nakaoka does not disclose or suggest storage and temper rolling of an ageing-sensitive steel. In view of these differences, Applicants respectfully submit that one of ordinary skill in the art would not have been motivated to modify the teachings of Nakaoka to arrive at the instant invention.

Applicants deem the rejection of claims under 35 U.S.C. § 103 to be obviated and respectfully request withdrawal thereof.

Applicants hereby respectfully request a two (2) month extension of time for responding to the Office Action. Please deduct any fees resulting from this Amendment from deposit account number 16-2500 of the undersigned.

In view of the foregoing amendments and remarks it is firmly believed that the subject claims are in condition for allowance, which action is earnestly solicited.

Respectfully submitted, PROSKAUER ROSE LLP

Bv:

Mitul I. Desai Reg. No. 46,661

July 16, 2001

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Enclosures: Appendix of Marked Up Version of Amended Claims

Exhibit A Exhibit B



APPENDIX OF MARKED UP VERSION OF AMENDED CLAIMS

- --1. (Twice Amended) A process for the production of a buckling-resistant stove-finished structural component from a cold strip which [consists of] comprises ageing-sensitive steel with a high bake-hardening potential, [more particularly of more than 70 N/mm²,] characterized in that
 - the cold strip is converted by [a dressing] temper rolling to a yield point elongation-free state in which the condition $R_{\rm eh}$ - $R_{\rm el}$ < 2 N/mm² is met,
 - the cold strip is then stored to storage temperature below room temperature for a storage period whose length is at most equal to the length of the period at whose end the value of critical ageing is reached which results in dependence on the particular storage temperature,
 - to storage the cold strip is cold worked to give a structural component, and
 - the structural component is [finally] stove-finished.
- --3. (Twice Amended) A process for the production of a buckling-resistant stove-finished structural component from a cold strip which [consists of] comprises ageing-sensitive steel with a high bake-hardening potential, [more particularly of more than 70 N/mm²,]

characterised in that

- the cold strip is stored undressed for a storage period at room temperature,
- following the storage period the cold strip is converted by [dressing] temper rolling to a state in which the condition R_{eh} R_{el} < 2 N/mm² is met, the [dressed] temper rolled cold strip is then cold worked to give a structural component, and
- the structural member is [finally] stove-finished.

Iron and Stee Dictionary

Deutsch - Englisch Englisch - Deutsch German – English English - German

> 7. Auflage 7th edition

EXHIBIT A

Herausgegeben vom / Edited by Verein Deutscher Eisenhüttenleute

STAHL CESEN

Drehwinkel-Mefigmformer

of rotation transducer

Speed

Drehwinkel-Meßumformer m angle

Drehzahl / number of revolutions;

58

dreitelliger Antahrkopl m threehead dumniy bar

Orelwaizengerüst n three-high rolling stand

Dreiwellenkumpensator m concertina-type expansion joint Dresslerblumen fol leathering Areseleren drass; level

Drasslaren n skin pass rolling; temper (pass) rolling

Dresslergerüst n skin pass rotting mill

Drosslerwalze / roll for skin pass rolling mill; skin pass roll

Drosslerwalzwerk n skin pass mill; temper (pass) mill; temper (pass) rolling mill

DRI n direct reduced iron (DRI) Drillingsguß m triple casting Drillknicken n torsional buckling Drillmoment n twisting mament Orillwuiststahl m Iwisted (reinforce-

ment] bulb steel Drop-Weight-Probe / drop-weight

trial Drossel / (elakir.) chaking coil;

reactance coil; throttle Drosselklappe / butterfly valve; throttle valve

Drossellaistung / (Lichtbogenolen) supplementary reactor rating

drossela choke; throttle Drosselspule / (Lichtbogenoten) line reactor (am.); supplementary reactor

Drosselventil a butterfly valve; choker valve; throttle valve

Druck m compression; pressure; Ibrust Druckabiali m pressura drop

Druckausgleichbabäller m surge

Druckbeanspruchung / compression load; compression stress; compressive stress

Druckbohälter m pressura vessel Druckbogon m sheet (printing) Druckbruch m compression fracture

drücken push; spin Dracken a spinning

Drücken n (Biachumforman) metal spinning Drücken a von Außenborden spin-

ning of external flanges Drücken a von Hobikörpera spinning of hollow items

Drücken a von Innanborden spinning of inside beads

Drücker in pusher Druckerausgabs / (EOV) print-out Druckarol / printing office Orackarolmaschine / printing machine

Druckerweichung / (II. Steine) spitening under load (refractory bricks)

Druckleder / pressure spring Drucklestigkeit / compression strength; compressive strength; crushing strength

Drucklestigkeit / (Werkzeugstähle) compression strength (tool steels) Druckleverbusiandigkelt / refractoriness under load

Druckflüssigkalt / hydraulic fluid Drucklörderer m dispenser Druckgasentschweleiung / desulphurisation of pressure gas Druckgebläse n forced draft fan

Druckgeläßversuch m pressure vossal tost Druckgleßkokille / pressure casting

mo[u]ld Druckguft m compression casting: Oruckschmierung

die casting; high prossure die

casting, pressure pouring Drackgufistack a pressure die casting

Druckhoha / head

Druckkessei m high pressure boiler; high pressure container, high pressure tank

Druckkraft ((Pressen) compressive force

Drucklager n thrust bearing Druckluft / compressed air Oruckiultanlage / compressed-air

system Drucklutt-Gesenkhammer m compressed air drop hammor

Drucklutihammer m compressed air hammor

Druckfulthärten a air blast quenching Drucklufthaber m air lift pump Drucklutikesset m compressed air

container: compressed air tank Drackiufiteliung / compressed als

Druckluffmaßgarat n pressure

Dintering and combies seq air tool; pneumatic tool Oruckmanial m pressure shell

Druckmarklerung / pressure mark-

Druckmaßdase / pressure cell Druckmesser m manomater; pressure ga(u)ge

Orackminderventil n pressure reducing valve

Druckmutter / screw-down nut Druckorobe / tension test Drugkpumpe / tarcing pump Druckregier m pressure gavernor

Ornekschmierung / forced lubrica-

Drehzahlablall m rpm drop; speed drap Drehzahlverlaul m speed characteristle Drehzapfen m pivot dreieckig three-cornered; triangular Dreieckschaltpunkt m delta connection drellach threefold Drei-Glocken-Gichtverschluß m three bell hopper arrangement Dreihunden-Grad (300 °C)-Versprädung / irreversible temper brittleness Drolkantschraube / triangle head cap screw Dreikantatahi m Iriangular section Dreilagenbiech o three-ply plate: triangular section Dreilagenstahl m three-layer steel: two sided clad steel Drellagenstahlblech n sott center steel sheet Orellochdüse / three-hole nozzic Oreiphasen-Sterngegenparaileischallung / three-phase star inverse parallel connection Dreipunitiblegeversuch m threepoint bending test Dreischichtbetrieb m ihree shift operation Dreistoffsystem n ternary system Oralairangmaschine / three strand machine Oreiziulenillier m (Spektralanalyse) three-stage transmission filter dreistulig ihree-stage; ihree-step

EXHIBIT A

Metals Handbook®

TENTH EDITION

Volume 1 Properties and Selection: Irons, Steels, and High-Performance Alloys

Prepared under the direction of the ASM INTERNATIONAL Handbook Committee

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First printing, March 1990

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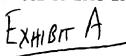
Library of Congress Cataloging-in-Publication Data

Metals handbook/prepared under the direction of the ASM INTERNATIONAL Handbook Committee—10th ed.

p. cm.
Includes bibliographical references and index.
Contents: v. 1. Properties and selection—
irons, steels, and high-performance alloys.
ISBN 0-87170-377-7 (v. 1)
1. Metals—Handbooks, manuals, etc.
1. ASM International Handbook Committee.
TA459.M43 1990
670 176—dc20 çm. 620.1'6-dc20

SAN 204-7586

Printed in the United States of America





Carbon and Low-Alloy Steel Sheet and Strip / 205

Tensile requirements for hot-rolled and cold-rolled plain carbon steel sheet and

2	Yield strength, minimum		Tensile strength,		Elongation in 50 mm
er grade	MP _e	kd	MPa	kd	(2 in.), minimum, %
anality hot-	olled sheet and strip is	cut lengths or	colls (ASTM A	570)(a)	
Man damen	205	30	340	49	25.0(b)
	230	33	360	52	23.0(Ъ)
	250	36	365	53	22.0(b)
	275	40	380	\$5	21.0(b)
Ř	310	45	415	60	19.0(b)
<u> </u>	345	50	450	65	17.0(Ъ)
	380	55	480	70	15.0(b)
	rolled sheet in cut leng	other our coile /AS	(a)(ttà A MT		
duality cold	Holled Street in car lens				
Ş.,	170	25	290	42	26
	205	30	310	45	24
	230	33	330	48	22
1 and 7	275	40	360	52	20
<i>1</i>	550(c)	80(c)	565	82	
A	casure vessels (ASTM A	414)			
			210	45	26(e)
US :		25(d)	310		24(e)
()	205(d)	30(d)	345	50 55	27(c)
A	230(d)	33(d)	380	55 60	20(c)
	240(d)	35(d)	415		18(c)
E	260(d)	38(d)	450	65 70	
¥3	290(d)	42(d)	485	70	16(e)
N	310(d)	45(d)	515	75	16(e)

is call products, tasting by the producer is limited to the end of the coil. Results of such tests must comply with the specified values, testing considerations must recognize that variation in strength levels may occur throughout the untested portions of the coil, the coil that variation is strength levels may occur throughout the untested portions of the coil, the product, the yield point approaches the tenalle strength and because there is no halt in the gage or drop in the beam. This find that is the tenal of the coil that is the product, the yield point approaches the tenalle strength and because there is no halt in the gage or drop in the beam. While product is the product of the coil that is the stress at 0.5% elongation, under load. (d) Yield strength determined by the 0.2% offset or 0.5% do number load methods. (e) At thickness, 1, of 3.7-5.9 mm (0.145-0.230 in.). Source: Ref 1

resistant to aging, are preferable to med and capped steels. For ingot cast-however, rimmed and capped steels are fally superior in inherent surface qual-ne lower in cost, and are preferred over disteel as long as the occurrence of other strains is not a problem.

Strain aging is related to the presence of nitrogen in solid solution in the steel and is affected by time and termperature, with longer times and higher temperatures producing greater aging. The strain-aging rate is also dependent on the amount of deformation that has occurred and is increased

when the deformati n occurs at higher temperatures or lower strain rates. Another important variable that affects strain aging is the amount of nitrogen in solution. Killed carbon steels have very little susceptibility to strain aging because their nitrogen content is essentially chemically combined with aluminum. Rimmed and capped steels, however, tend to strain age because they contain greater amounts of nitrogen in solid solution (typically 6 to 30 ppm).

Control of Flatness

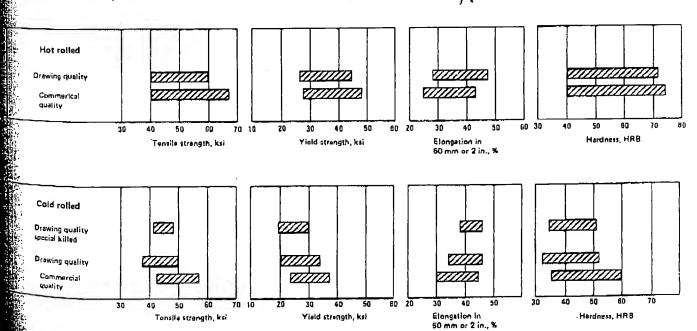
Plain carbon steel sheet is ordinarily sold to two standards of flatness:

- Commercial flatness, which is used where flatness is important but not critical
- The stretcher-level standard of flatness, which is required when little or no forming is to be done and the product is required to be flat and free from waves or oil can, or when flatness is necessary to ensure smooth automatic feeding of forming equipment

The permissible variations for the flatness of hot- and cold-rolled sheet have been established by the Technical Committee of the American Iron and Steel Institute and are given in the AISI Steel Products Manual. Commercial flatness can usually be produced by roller leveling or by temper rolling and roller leveling, but where very flat sheet is required, producers may have to resort to stretcher leveling, tension leveling, or other leveling processes.

In temper rolling, the steel is cold reduced, usually by 1/2 to 2%, which is also





NPIcal mechanical properties of low-carbon steel sheet shown by the range of properties in steel furnished by three mills. Hot-rolled sheet thickness from 1.519 3.415 mm (0.0598 to 0.1345 in., or 16 to 10 gage); cold-rolled sheet thickness from 0.759 to 1.519 mm (0.0299 to 0.0598 in., or 22 to 16 gage). All cold-rolled grades temper pass. All grades were rolled from rimmed steel except the one labeled special killed. See Table 5 for the mechanical properties of structural (physical) met.

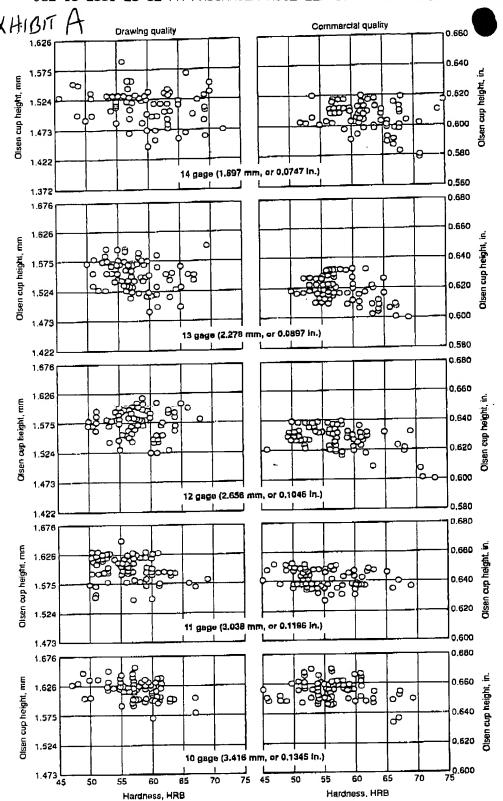


Fig. 2 Scatter in Olsen ductilities of hot-rolled low-carbon steel sheet

effective for removing yield point elongation and preventing stretcher strains.

In roller leveling, a staggered series of small-diameter rolls alternately flexes the

steel back and forth. The rolls are adjusted so that the greatest deformation occurs at the entrance end of the rolls and less flexing occurs at the exit end. Stretcher strains can also be climinated by roller leveling, as the deformation is great enough to move yield point elongation. Dead-soft nealed sheet cannot be made suitable production of exp sed parts by rollering because the rolls kink the sheet selly, producing leveler breaks. The deformareas or kinks will not deform further stretching and will appear as braised after forming.

Stretcher Leveling. Leveling by stretch cut lengths of the temper-rolled lengthwise between jaws (stretcher ing) is a more positive means of prodi flatness. Elongation (stretching) di stretcher leveling may vary from about 3%, which exceeds the elastic limit of steel and therefore results in some per nent elongation. The sheet must be killed or a capped steel having nearly form properties so that it will spring uniformly across its full width and ren flat. It may be necessary to use killed having nearly uniform properties so after stretching, strain markings do not velop.

Tension Leveling. Another flattening cess that is used for steel sheet is enleveling, which combines the effect stretcher and roller leveling. The sheepulled to a stress near its yield point which is simultaneously flexed over small the combined tension and bending prolivielding at the flex points.

Modified Low-Carbon Steel Sheet and Strip

In addition to the low-carbon steels and strip products already discussed interacticle, there are numerous additional puts available that are designed to say specific customer requirements. It products are often made with low-casteels having chemical compositions all y modified from those discussed earlies.

To be considered a plain low-cargrade, a steel should contain no more 0.25% C, 1.65% Mn, 0.60% S, and 0 Cu, but it may also contain small amount of other elements, such as nitrogen, play phorus, and boron, that are effective imparting special characteristics when ment singly or in combination. The modulow-carbon steel grades discussed before designed to provide sheet and approducts having increased strength, (ability, and/or corrosion resistance.

Carbon-Manganese Steels. Manganese solid-solution strengthening element interite and is also effective in increasing henability. Manganese in amounts range from 1.0 to 1.5% is added to low-carsteel (0.15 to 0.25% C) to provide characteringth (yield strength of about 275 or 40 ksi) with good ductility in hot-mand cold-rolled sheet and strip. Comments fabricated from these higher-mannese steels can be heat treated by quence.

HIBIT A

ab ut 4 to 6% reduction. However, if the

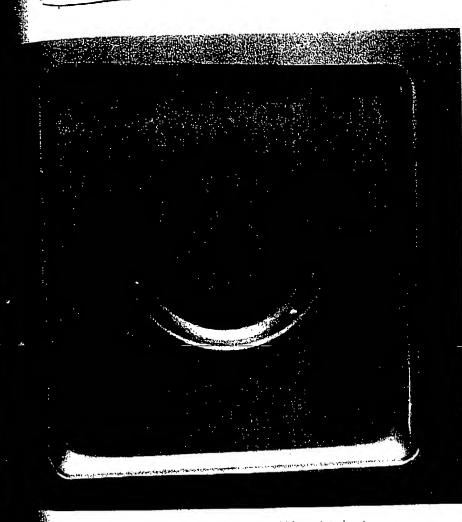
Embrittlement of Steels / 693

material is not formed within the safe period, discontinuous yielding will eventually return and impair formability.

Results of ne study illustrate the influence of strain aging on mechanical properties (Ref 32). Three steels made by different processes were evaluated: Steel A. silicon and aluminum deoxidized steel; Steel B, capped open hearth steel; and Steel C. capped Bessemer steel. Steel C had the highest nitrogen content. Steels B and C had low aluminum contents, while steel A had sufficient aluminum to tie up the nitrogen. Strips of each were normalized and loaded in tension to a permanent strain of 10%. The strips were held at 25, 230, 480, and 650 °C (75, 450, 900, and 1200 °F) for various lengths of time (≤25 000 h at 25 and 230 °C, or 75 and 450 °F; ≤10 h at 480 °C, or 900 °F; and 2 h at 650 °C, or 1200 °F). Hardness, tensile properties, and impact properties (half-width Charpy V-notch specimens) were determined at different aging_times.

Figure 10 shows the impact test results for steels A, B, and C strained 10% in tension and aged at room temperature up to 25 000 h. The impact curves are shifted with aging at room temperature for all three steels; steel A exhibits the best aged toughness, and steel C the poorest. Figure 11 shows the increase in hardness for steels A, B, and C aged for times up to 25 000 h at 25 °C (75 °F) and 230 °C (450 °F). Room-temperature aging produced a gradual increase in hardness with time. The maximum hardness was about the same and was reached quickest by steel C and slowest by steel A. The hardness increase with aging at 230 °C (450 °F) was constant for steel A and slowly decreased with aging for steels B and

In low-carbon steels, strain aging is caused chiefly by the presence of interstitial solutes (carbon and nitrogen), although hydrogen is known to produce a lesser effect at low temperatures. These interstitial solutes have high diffusion coefficients in iron and high interaction energies with dislocations. The change in mechanical properties of low-carbon rimming steels with different carbon and nitrogen contents that were prestrained 4% and aged various times at 60 °C (140 °F) has been demonstrated (Fig. 12) (Ref 34). This work clearly demonstrates the detrimental influence of higher carbon and nitrogen contents on strain aging. The solubilities of carbon and nitrogen in iron Are quite different. Nitrogen solubility is high in the temperature range where rapid precipitation occurs; the solubility of carbon, in equilibrium with cementite, is very carbon at temperatures below 100 °C (210 °F) is insignificant. However, above 100 °C (210 °F), & carbide can redissolve and produce substantial strain aging (Ref 35). Strain aging attributable to nitrogen is caused by



nple of stretcher-strain marks (LOders bands) on a cold-formed steel part

and may be isomorphous with it can With aging, the low-temperature ill gradually be replaced by Fe₃C The phase changes during aging of gen and iron-carbide quench aged ediscussed in the literature (Ref

ge Embrittlement

aging occurs in low-carbon steels certain amounts and then aged, oduces an increase in strength and but a loss in ductility (Ref 25-27, he degree of deformation, or cold important. Generally, about a 15% in thickness provides the maxi-The resulting brittleness varies ging temperature and time. Aging emperature is very slow, requiring nonths to obtain maximum embritas the aging temperature is inic time for maximum embrittleases. Certain coating treatments, or dip galvanizing, can pr duce a ce of embrittlement in areas that worked the critical am unt; this brittle fractures. To prevent this

problem, the part can be annealed before galvanizing. Alternatively, the use of sheet steels containing elements that tie up nitrogen, for example, aluminum, titanium, zirconium, vanadium, or boron, will prevent strain-age embrittlement.

Strain aging may also lead to stretcherstrain marks (Luders bands) on coldformed low-carbon sheet steel components. These marks are cosmetic defects, rather than cracks, but their presence on formed parts is unacceptable (Fig. 9). During tensile loading, sheet steel that is susceptible to this defect will exhibit nonuniform yielding followed by uniform elongation. The elongation at maximum load and the total elongation are reduced. decreasing cold formability. In a nonaluminum-killed sheet steel, a small amount of deformation, typically 1% reduction, will suppress the yield point for several m nths. This process is referred t as Now. Therefore, strain aging that is due to roller levelling or temper rolling (Ref 31)

This process is more effective in eliminating the sharp yield point and preventing strain aging than stretching the steel through the Lüders strain, which requires

OSCAR BRANDSTETTER VERLAG · WIESBADEN

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DICTIONARY

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Fünste, vollkommen überarbeitete und erheblich erweiterte Auslage

Ernst, Richard:

Verfahren, Richard Einal. - Wieduken: Brazistetter Teilm, mit Parallelsscht, ensprechend d. Sprache weitgehender Berüchs, d. neuzeitl. Technisten v. A oree chuch der indintriellen Technik.; wirer

d. Bd.: Dictionary of industrial technics -Dictionnuire de la technique imbustricle.

Orcionario de la termes industrial. – Decorativo da técnica industrial ab Ba. 9 u. d. T.: Ernsi. Richard.; Comprehensio decionary

of engineering and technology

8d. 2. Englisch-Deutsch, – S., vollkommen eberach, u. erhach, erw. Auft. – 1985. ISBN 3-87097-116-9

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S. Auflage 1985

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Der Umbruch wurde mit Programmen der RZB Rechenzentrum Buchhundel GmbH gerechnet Texuverarteitung: Siemens-Programmsystem-TEAM Lichtsatz: dateam Vertriebsgesellschaft mbH + Co. KG, Frankfurt am Main Druck: Oscur Brandstetter Druckerei GmbH & Co. KG, Wieshaden

Library of Congress Catalog Card Number Af 28085

9-911-79078-E NBSI

Printed in Germany

zwei Seitenläuhen gleichzeitig früden 1 - milli

vom (o. im) Lager, Warenlager #1.*, warehouse / Speicher m. Lagerhauv m. -taum m. Lager n. Magazin #1.*, shop (US) / Laden m. Geschältsbokul #1 on ~ / auf Lager 1.* access (GB) a. fegen (* 1. accumulaie / speichern. aoxamineln (* keep / aufhowahren, aufhoben (* mature / ablagern (* (comp) / einspeichern. store of warehouse of Cagero, and Lager nehmen Lagervorrat, -bestand m. Inventar n. Material ni - yard - Lager n. -platz m; - yard flumben / cintesent in bulk / lose lagern 1 - n (compl / storay, levant storay (phurm) / Storay and oil / Stapetplatz m1 - zone of data (comp1 -Storaxöl n. - tree / Benzuebaum m store-and-forward mode (compl / (ramp) / Speicherzugriff m Speichermane / für Daten

store back (comp) / wiedereinspeichern i - construction / Ludenbuu ml - controller (comp) heat / Speicherwärme fl. program computer / speicherprogrammiester Rechner I - program controlled. SPC / speichergesteuert I - program system, SPS / speicherprogrammiertes System, machine / Kondensatorfschweiß]maschine / Speichervermitlung (1 - service lieleram)/ Nitteilungsdienst mil - stulteblug center / Speichervermitlungsstelle (/ Lagerkontrolleinheit f

/ Lagerschuppen m. Materialschuppen m. |- fank / Vorrasschülter m. |- timber / Stapelholz n. · up, stockpite / nufstancin, -speichern! · up heat Lugeruulscher, -verwalter m. (auch.) -arbeiter m) -s label / Werksloffkurte f, Materialkarle f Lagerraum m. Lager n. Werkzeuglager n. 1 shed dore house / Lugerhaus n1 - keeper o. man / - lumber / Stapetholz n: - room for tools / storey (GB) (en engl/Stockwerk n. Sinck m. (Schweiz)] - losses / Lagerverhiste m pl / die Würme binden o. aufspeichern

m. Speicherung (1 - properties / Lagerfühigkeit f atmusphere / Feuchtlagerung fl > of water / Stau Lagerlungs)temperatur (i > under mask (comp) / Speichern numer Maske Speicherbecken, Speischecken n1 - in a sito / Einlagerung / im Sito, Silieren n1 - in humld storward / Materiallagerplatz an storward garden level / Gartengwechoß n storing / Lagerung / (von Güttern) (- (wmp) / Speichern 11 - basin o. wservoir o. (ank / 1 - routine teampt / Abspeicherroutine /f - temperature (uarchmeel /

unserbringung f

pasement (dam) / Büschungspillister n.g. sewage storm flow (mad) / Regenwasserahfluß m1~guyed Oberflüchenwasser-Kanadisation G vignal / HochwasserJurchfluß, Notauslaß m 1 - water Sturmhall m? - warming - Sturmwarmung A pole (telecom) / Linicolestpunkt m (* ladder Lausentreppe f, Sturmleiter f, Seefulfreen n. Oberflächenwasser n. vater flow fhydrid Regenwasser n. Oberflüchenwasser n. Regenvasserkunal mits sewer system. -water / Recenwasser ii (Abwasser). (Abwasser)** sewer, worm deain / Störmer unit / Störmer-Einheit f

Portalhubwagen m, stapler m, stapelwagen m. Isinapler, Jader m. Van Carrier mix-mill v./

Ahliufspeicher mit - word leempl : Speicherwon

Warmwasserspeicher in Entleerungs-

Buhrang fauf der Mittellinie? - Joader o. lift /

Gerkran m Psculter (m tookl)

EXHIBIT

Anaummlungshehalter, stank m! - window, storm story (US) teis engl / Surchwerk n. Stock m. Geschob radk o, reservoir / Regenklär, -wasserhecken n. sash / Varfenster at

temper 1. Jeanmell einbrennen 1. (tet.)

temper 1. Jeanmell einbrennen 1. (tet.)

reduzierend bleichen, schwefeln 1. dry (tex.)

kammertocknen 1. hew.). Darre (1. (CB), stove

kinnaue framel). Einbrennofen m. (CB),

greenbouse / Gewärelshaus n. 1. kitchen nange

Kächenken m. Kochherd m. 1. kitchen nange

(ES) / Schliteschraube fmit Metallgewinde

(Rundkogf o, versenkt), Senkschraube mit - cloth / dichtes fo. starkes o. schweres) Tuch shattering (civ eng. concrete) / enge Schalung l storoine ichem) / Stovain n. Amylocain n store vi / im Warmenfen trocknen [- (plust) / stout n (brew) / Stoutbier n. Stout m 1 > adj/ gedrungen, stark, fest 1 - close-boarded ingsschlitz, Rundkopischraube mit

store drying (tex) / Kammertrecknen nt Senamel v. Ofenheizung für pipe / Ofenrohr al - pipe elbow forming machine / Knierchröiegemaschine fl -roam / Heizungsnum, keller m f. room (brev) / Durce ft - setting / Kaminksu 1018 - file / Einbreanlack m. eingebrunnter Luck 1. fillings Imen./ Winder hitzerbesalz m. Cowperbesalz ml. filter o. maker o. setter / Ofenselzer mt. - heating (cir engl./ Einzelofenheizung f. Lanasschitz storeid-enamet linish, stove enameling Ofenkachel f. Kachel f Einbrennlackierung (

ariste (minag) / wegraumen sjonage (shipt / Nauumg // Verstauen n.1 - (mining) / storing text) / Schwefeln n. Schwefelkummerbleiche f. Schwefelbleiche fl. (paint) / Einbrennen n3 > (plast) / Nachhästen n1 > ehamber (txx) / Schwefelkummer II Stanfaktor, -koeffizient m. Raumte fiin m'/t) ! sequipment (lex) / Schwefelbleich-Gerate a pl -loop (parachue) / Parkschlaufe /l - of useful ston, pack (mining) / versetzen, zukippen ; > put Bergeveranz Versuz m?-factor (ship)/ load (space) / Nutslasshefestigung f.-

machine [mining] / Versutzmaschine /i > plpe fine itraddle 11. span (e.g. a civer) / lim Reishiz)
uberspannen (f. (US) (ingallanen) / umgehen,
ausweichen (f. - the Inad / die Cast überfahren) Portalhubwagen m. Portalishrzeug ni - crane / pneumalic type / Błasycrsatzmaschine f S.T.P., s.r.p. (thermalyminis) = almdard umperature Bergeversatz, Versatz mil > machine (mming) / Versatzmaschine fl. marhine, centrifugal o. stowed (space, appendage) / cingexogen stower (mining) / Versil zarbener 111) -, stowing Schleuderversatzmaschine f! - muchine. stowing thydr) / Anstauung fi - (miningl / ritmill / spreizen i > carrier o. truck / Forhubwagen, Torstapler, -Inder m. stow away / unterbringen, verstauen (mining) / Hasrohrheitung / niechanical type (mining) / ite. - stroke | > - steamer

schnurgerade jin a hine / schnurgerade ;

- accent (gaph) / Lingvezichen ol - anybitie d

- accent (gaph) / Lingvezichen ol - anybitie d

Geradeusverstänken ml - angle / gestrekte O

Winkel :- arch tor teg! / Flachgewöll

stenghlang, tmelhol! / direkt, rein | - st

Geradstich m.

straffat axle (rail) / gerade Achse. Normulachx | D

straffat axle (rail) / gerade Achse. Normulachx | D

straffat axle (rail) / gerade Achse. -barrel sault Halbkreisgewölle a.
Tonnengewölle n 1 - bead twelst, Längsraht toner eigen mit 200 bet rivet Riemenniet mit 200 bevel gear / D. Kegelstinnudgerteibe n 2 - binary / rein hin in binst (umary gas / unvernisches Huchof flight; carbon steet / Exist review restriction and carriage limiters district results of the carbon, Fuchsschwarz m. 1 - bank o. muhiple (telecom gerudes (o. unverschränktes) Vielfachfeld. > O knitting muchine / Cousonmuschine I. O Flachkuliermaschine I/ - bar linking machin III. onso minary pas / minamina inamina | 0 | - bobbin tysinii / Tellerspuie / Randspuie / 0 | - bow teir engl / gerader Bagen. Sturckwegen / 0 | Show the cight germans organised branch of the property of the connection of lead pipes / gerald Nerhindung was Bleirebreak - brick / O Normalacia and Shrick Interface (Normalacia and Shrick Interface) of the cight of the property of the cight of the c crossfall noad / Palquerschnitt m? - eu Berinding wheel / zylindrischer Schleistops - Kenning spenil (LS) (S. Streekensteue - J. Gening spenil (LS) (S. Streekensteue) seylindrical pin / Padstiff m.t. differentia E Arafing Inni im Tieffluy Angreilen Straggling navii / statistische Streuung. Stragglin Site et die f. Streubreite f. Straggling Site of Straggling (ex.) / Flachkettelmaschine f.-kettmaschine f.)

- bar machine (tex.) / Flachketek meschine f. T. Wischelmer (help n) verble truffet / getall – Kahetahgang (verp jewel telsek) / Oceksten O (stain) / gerade, geradläufig) - (substance) / fel 🕜 un ermischi (- (liquids) / unverdünni (- upri 🔾 Gabelschlussel in für Kreuzlich o. Nutmute fa- extindeical grinding / Durchschleifen ... flach : verban steel / remer Koddenstoffu: traightedge ideast/ Lineal a. Linienzieher / - cut positioning (N/C) : Streckenposition Einzug - deequiff / einbeitlicher Farbstol stroigh a surs) Zwischengrade (Tzwischen Krümmungen) 1 – adj / gerade, geradling) – (suirs) gerade, geradiärlig i – substance) / et j gegna. Hardingal n. Abrightlingal n. Tuschierhusal n.is Brikerleiweigts Abr f. Riebissheit n. / scheiteltecht, aufrecht f / Igis) / unvermisch (oil) / nichwassermischbar i in a - line / (DIN) - deavingsia draft (spias) / gerader straddling dowel / Spreizdübel m f. position / Stradillepacker mi - the cantinuous ling Imai - wrench, face wrench for slutted lock rings / scontinuous (will) rein kontinuierlich ! Stelyradschlepper m 1 - truck see straddle carrier Franco n zweier Seitenflächen : > packer foll, colly and dem Strich reston 1 - tractor tagel / schnurgerade lin u - line / schnurgerade i Normalacia m?~ buttonbole (sea m17 Reitsitzstellung ft - rincyard tractor / - back hand saw with open handle Weinkulturgeral nauf Sielzen Deppelscheibenfräser m3×habe over center line /